FINAL DRAINAGE REPORT

Prepared for:

Alkemista Café & Bar 2144 W. State Route 89A Sedona, Arizona 86336



December 21, 2021

Prepared by:









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I. GENERAL LOCATION AND DESCRIPTION

A. Project Location

The proposed development of Alkemista Café & Bar is a commercial development that will be located within the incorporated City of Sedona, Yavapai County, Arizona. More specifically described as Assessor Parcel Number (APN) 408-24-070A and 408-24-070C in a portion of the Southeast ¼ of the Southeast ¼ of Section 11, Township 17 North, Range 5 East of the Gila and Salt River Base and Meridian. The property is located northeast of the intersection of State Route 89A and Goodrow Lane. The proposed access point to the development will be located off Goodrow Lane.

B. <u>Property Owner/Developer</u> Sergio Goma Properties

2144 State Route 89A Sedona, Arizona 86336

C. Description of Property

The proposed development of Alkemista Café & Bar will consist of four (4) new buildings to replace the existing three (3) building within the property. The development encompasses approximately 0.89 acres and is currently developed. The property is currently zoned as Commercial (CO). Surrounding zones are Single-Family Residential (RS-10) to the North, Lodging (L) to the west, and Commercial (CO) to the east. The proposed usage will be Commercial.

The general soil condition is classified as "Upland Sandyloam" which is Natural Resource Conservation Services (NRCS) Hydrologic Soil Group 'B' soil with an estimated 40% vegetative cover consisting of desert brush and grasses. NRCS Type 'B' soil is typically characterized as highly fine, sandy loam which has a high rate of infiltration therefore a low runoff potential. The existing topography of the property is moderately sloped with an average of 2 to 5 percent grade in a northeast to southwest direction within the upper portion of the property, and a southeast to northwest direction within the lower portion of the property. There are no irrigation facilities within the property.

The property is not situated within any designated FEMA Special Flood Hazard Areas as indicated in the current FEMA Flood Insurance Rate Map (FIRM) No. 04025C1435G, effective September 3, 2010. The property does fall within the City of Sedona designated 100-year floodplain as identified as Profile 4100 within the City of Sedona Floodplain Management Study dated May 1994.

D. Previous Studies

The property is included in the following drainage studies, but it should be noted that the hydrologic methodology used in this drainage report is specifically for this property and do not override previous studies. The following studies were used as reference for this drainage study:



- City of Sedona Floodplain Management Study prepared by USDA Soil Conservation Services, dated May 1994
- ii. City of Sedona Stormwater Master Plan prepared by Dibble & Associates, dated March 2005.

II. DRAINAGE BASINS AND SUB-BASINS

A. Major Basin

The proposed development falls within a portion of the Coffee Pot Drainage Basin as delineated within the City of Sedona Stormwater Master Plan Study. The drainage basin has a contributing area of 0.24 square miles and concentrates near the western property boundary near the inlet of the existing 4-foot diameter culvert crossing Goodrow Lane. The drainage basin is comprised of three delineated basins identified as B59B, B60B and B61B within the Coffee Pot Drainage Basin of the City of Sedona Stormwater Master Plan Study. Runoff flows through the basin is through developed and undeveloped areas consisting of shallow overland flows to well-defined drainage paths.

The drainage basin was divided into an off-site sub-basin and an on-site sub-basin. The on-site sub-basin encompasses the Alkemista Café & Bar development which is approximately 0.87 acres. Currently, runoff through the on-site area is within a well-defined channel running in an east to west direction to the existing 48-in. diameter beneath Goodrow Lane. The off-site sub-basin encapsulates the off-site runoff flows that will enter the property along the eastern and northern property boundary.

B. Minor Basin

For a hydrologic analysis of this development the on-site sub-basin was evaluated for the pre-development and post-development conditions.

III. DRAINAGE DESIGN CRITERIA

A. Hydrologic Analysis and Results

i. Methodology

The methodology used for this hydrologic analysis was based on the Rational Method as described within the Arizona Department of Transportation Drainage Design Manual. The hydrologic modeling software HydraFlow Hydrographs was used to calculate the runoff for the pre-development and post-development conditions. The hydrologic methods used within the previous drainage studies are not the same methods used for this drainage study. The hydrologic calculations used within this report will be used for addressing the post-development design conditions in comparison to the pre-development hydrologic conditions. This report does not override any previously accepted studies by the local jurisdiction.



Rainfall intensities were derived from the rainfall depth-duration frequency statistics from NOAA 14 Precipitation-Frequency Atlas and Table 3-2: Mean Precipitation Frequency Estimates within the City of Sedona Design Review, Engineering and Administrative Manual.

The Time of Concentration was estimated using equation 2.2 within the ADOT Drainage Design Manual

The Runoff Coefficient was derived using Figure 2-1 for the developed areas. The on-site sub-basin which is partially developed was determined to have a runoff coefficient of 0.58 for the pre-development condition and 0.90 for the post-development condition.

ii. Hydrologic Results

The on-site sub-basin, containing the Alkemista development, was evaluated to determine the difference between the pre-development and post-development hydrologic conditions.

Table 3.1 Summary Discharges

| DISHARGES (cfs) | | | | | | | | | |
|--|------|------|------|------|------|------|--|--|--|
| 2-yr 5-yr 10-yr 25-yr 50-yr 100-yr Sub-Basin Peak Peak Peak Peak Peak Peak | | | | | | | | | |
| Pre | 1.28 | 1.72 | 2.09 | 2.62 | 3.06 | 3.54 | | | |
| Post | 1.99 | 2.68 | 3.24 | 4.06 | 4.75 | 5.49 | | | |

As a result of the development and the increase in impervious area, there was in an increase in the peak discharges between the pre-development and post-development conditions.

The following table shows the discharges with the proposed mitigation as described later in this report.

Table 3.2 Summary Discharges with mitigations

| DISHARGES (cfs) | | | | | | | | | | |
|-----------------|------------------------------------|------|------|------|------|------|--|--|--|--|
| | 2-yr 5-yr 10-yr 25-yr 50-yr 100-yr | | | | | | | | | |
| Sub-Basin | Peak | Peak | Peak | Peak | Peak | Peak | | | | |
| Pre | 1.28 | 1.72 | 2.09 | 2.62 | 3.06 | 3.54 | | | | |
| Post w/ | | | | | | | | | | |
| Mitigation | 1.21 | 1.50 | 1.75 | 2.14 | 2.50 | 2.84 | | | | |





Using the City of Sedona Stormwater Master Plan, the 100-year and 25-year peak discharge from the off-site sub-basin entering the on-site basin is 565 cfs and 422 cfs respectively. A portion of the off-site flows will be contained within the existing stormwater system in the adjacent commercial development to the east and enter the property thru a 4'x4' box culvert. The existing hydraulic conditions of the stormwater system to the east is unknown but based on typical flow conditions for 4'x4' box culvert, we assume the stormwater system will contain 300 cfs. Peak discharges above 300 cfs is assumed to enter the on-site sub-basin as overland flows with no specific concentration point. As noted previously, the development is within a 100-year floodplain as shown within the City of Sedona Floodplain Management Study.

B. Hydraulic Analysis

- i. A hydraulic analysis of the proposed 48-inch diameter culvert was not performed since the amount of off-site flows contained within the existing stormwater system in the adjacent commercial development to the east cannot be confirmed. The installation of the new 48-inch culvert within the proposed development would require connecting the existing 4'x4' box culvert on the east property boundary to the existing 48-inch culvert on the west property boundary. It should be noted that the existing 48-inch culvert along the west property boundary beneath Goodrow Lane is undersized and is not able to contain the 100-year storm event and the 10-year storm event as determined within the City of Sedona Floodplain Management Study for Profile 4100.
- ii. Since the proposed development lies within a City of Sedona designated 100-year floodplain a HEC-RAS model was developed to determine the depths of flow across the development. The off-site discharge of 565 cfs was applied to a topographic surface developed from the City of Sedona GIS data and the proposed development grades. The hydraulic model illustrates storm discharges that exceed the capacity of the existing 4'x4' stormwater system in the adjacent commercial development will by-pass and enter the development along the north property boundary as shallow overland sheet flow. The approximate depth of flow entering the development ranges from 6 inches to 18 inches which continues across the development to the west property boundary. The 100-year peak discharge flows were determined to effect only one building within the development. The proposed building along the western property boundary adjacent to Goodrow Lane, identified as Building #4 in the construction plans, was determined to have a depth of 0.75 feet. The 100-year Base Flood Elevation upstream of Building #4 is therefore 4403.42 feet.



IV. DRAINAGE FACILITY DESIGN

A. General Concept

- i. The proposed development of Alkemista Café & Bar resulted in an increase in the pre-development peak discharge leaving the site. The increase in the peak discharge can be attributed to the increase in impermeable area because of the development. To reduce the peak runoff leaving the site an underground detention basin was implemented on-site. Runoff from the on-site basin will be directed to the underground detention basin for storage and attenuation.
- ii. A portion of the proposed development lies within a 100-year floodplain and therefore any structures that fall within the boundaries of the flood hazard area will be elevated 1-foot above the determined Base Flood Flevation.
- iii. To convey the off-site runoff from the existing 4'x4' box culvert a 48-inch diameter culvert will be installed to extend from the box culvert to the existing 48-inch culvert along the western property boundary beneath Goodrow Lane.
- iv. For post construction stormwater management to minimize water quality impacts from the development the proposed underground detention basin will be used for storage and filtration of all on-site runoff flows from paved areas. The crushed stone and underlaying storage area will be sized to treat the initial First Flush volume from the development. First Flush is defined as the first half inch of runoff from the developed area. The crushed stone will provide removal of sediments, and other non-point source pollutants from the development along with removal of petrochemicals and hydrocarbons within the parking lot area. This system is compliant with the Arizona Pollutant Discharge Elimination System (AZPDES) permit and the City of Cottonwood regulations.
- v. During the construction phase of the development storm water quality will be managed as specified within the Storm Water Pollution Prevention Plan (SWPPP) included within the approved construction plans.

B. Specific Details

i. For post construction storm water quality management and post-development attenuation, runoff flows from the on-site sub-basin will be contained and filtered within proposed underground detention basin. The basin will have a total storage capacity of 1,644 cubic feet for runoff storage within the 5-feet deep underground crushed stone storage area excluding the area for the 48-inch diameter culvert. The crush stone storage area will be lined with a filter fabric to separate the crushed stone and the natural soil to maintain a separation between



the two types of media. A 6-inch and 4-inch perforated PVC pipe will be embedded within the crushed stone to provided filtered drainage out of the basin. The required First Flush volume to be contained is 1,582 cubic feet. The basin has a crushed stone storage area of 1,644 cubic feet for containment and filtration. Running thru the 5-feet deep by 9.6-feet wide crushed stone storage area will be a 48-inch diameter culvert which is only to convey the off-site runoff from the existing 4'x4' box culvert thru the development. The 12-inch laterals used to direct flows from catch basins within the basin will feed directly into the crush stone storage area and not tie into the 48-inch diameter culvert.

- ii. To convey the off-site runoff entering the development from the existing 4'x4' box culvert, a 48-inch diameter HDPE culvert will be installed connecting the box culvert with the existing 48-inch diameter culvert beneath Goodrow Lane. The culvert has a length of 161 linear feet and a maximum slope of 13.3 percent.
- iii. Building #4 located along the western property boundary adjacent to Goodrow Lane has a determined Base Flood Elevation of 4403.42 feet. The Finished Floor Elevation of the building will be at a minimum 4404.42 feet since it is located within a flood hazard area.

V. RECOMMENDATION AND CONCLUSION

It is the engineer's recommendation that the site be developed as proposed. The plan will satisfy the conditions for design while maintaining a cost-effective, low maintenance drainage facility. The facility will mitigate any anticipated increase in runoff up to the 100-year storm event because of the proposed development. The facility follows the standards and regulations of the City of Sedona.

- The post-development 100-year peak discharge with mitigation from the development is **2.84 cubic feet per second** which is lower than the pre-development 100-year peak discharge of **3.54 cubic feet per second**. The peak discharge occurs along the western property boundary at the inlet of the existing 48-inch culvert beneath Goodrow Lane.
- The increase in runoff flows because of the development was attenuated through thru an underground detention basin. Post-development Runoff flows from the development were directed to the basin for attenuation and treatment.
- Post construction stormwater quality management was achieved using underground crush stone storage areas sized to contain the First Flush volume.
- A 48-inch diameter culvert will be installed to capture and convey off-site flows from the
 existing 4'x4' box culvert thru the development. The culvert will extend from the east
 property boundary to the existing 48-inch culvert beneath Goodrow Lane along the west
 property boundary.
- Building #4 will have a minimum Finished Floor Elevation of 4404.42 feet.

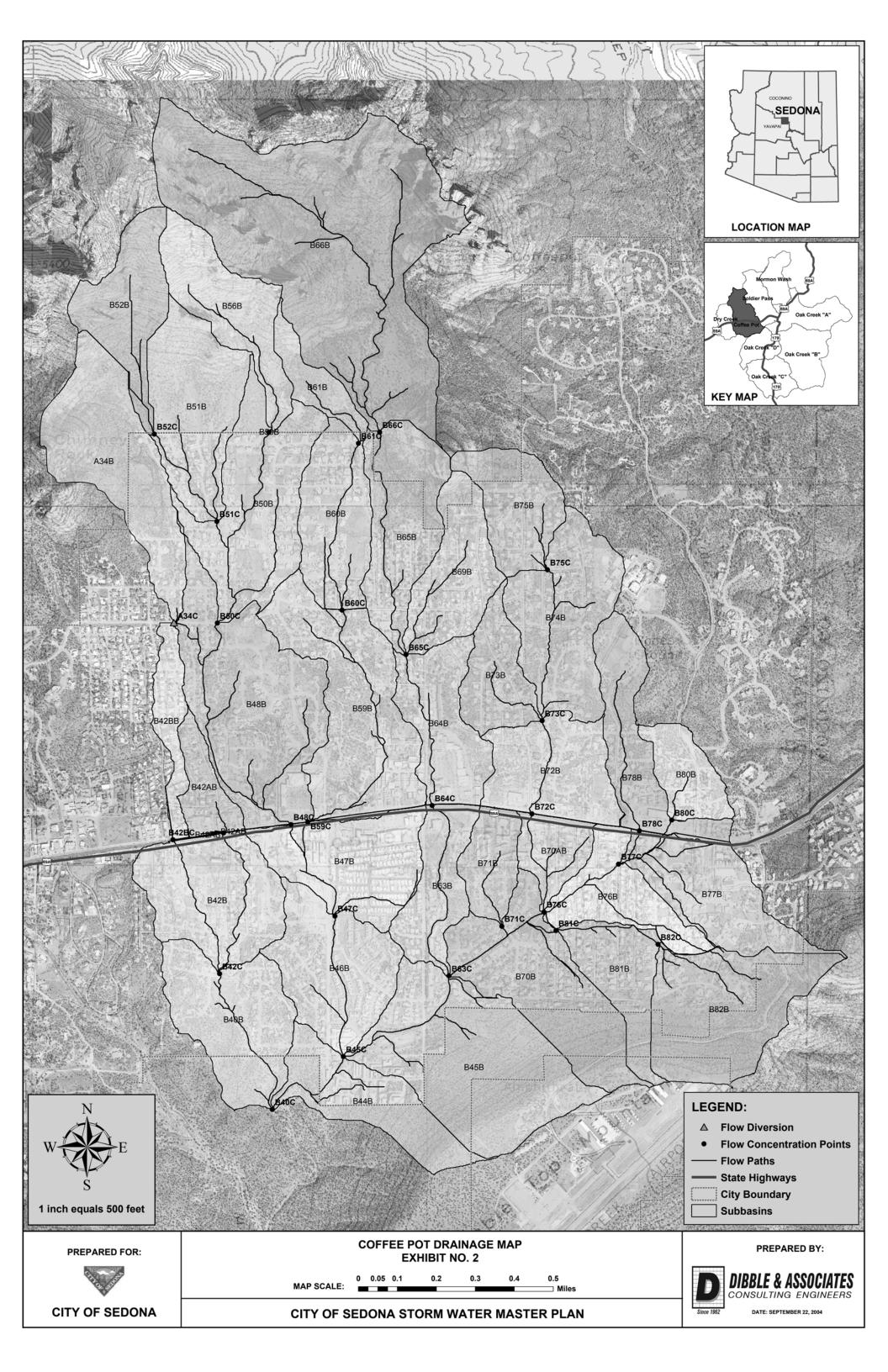




- The proposed storm drains and detention basin will be services and maintained by the developer. The devices and basin should be inspected on a quarterly basis or after significant rainfall events.
- No additional county, state, or federal permits regarding drainage is anticipated or required at this time.

Appendix A

| City of Sedona Stormwater Master Plan Excerpts |
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SECTION F.2A Coffee Pot HEC-1 Model Summary Output (25-Year, Future Condition)

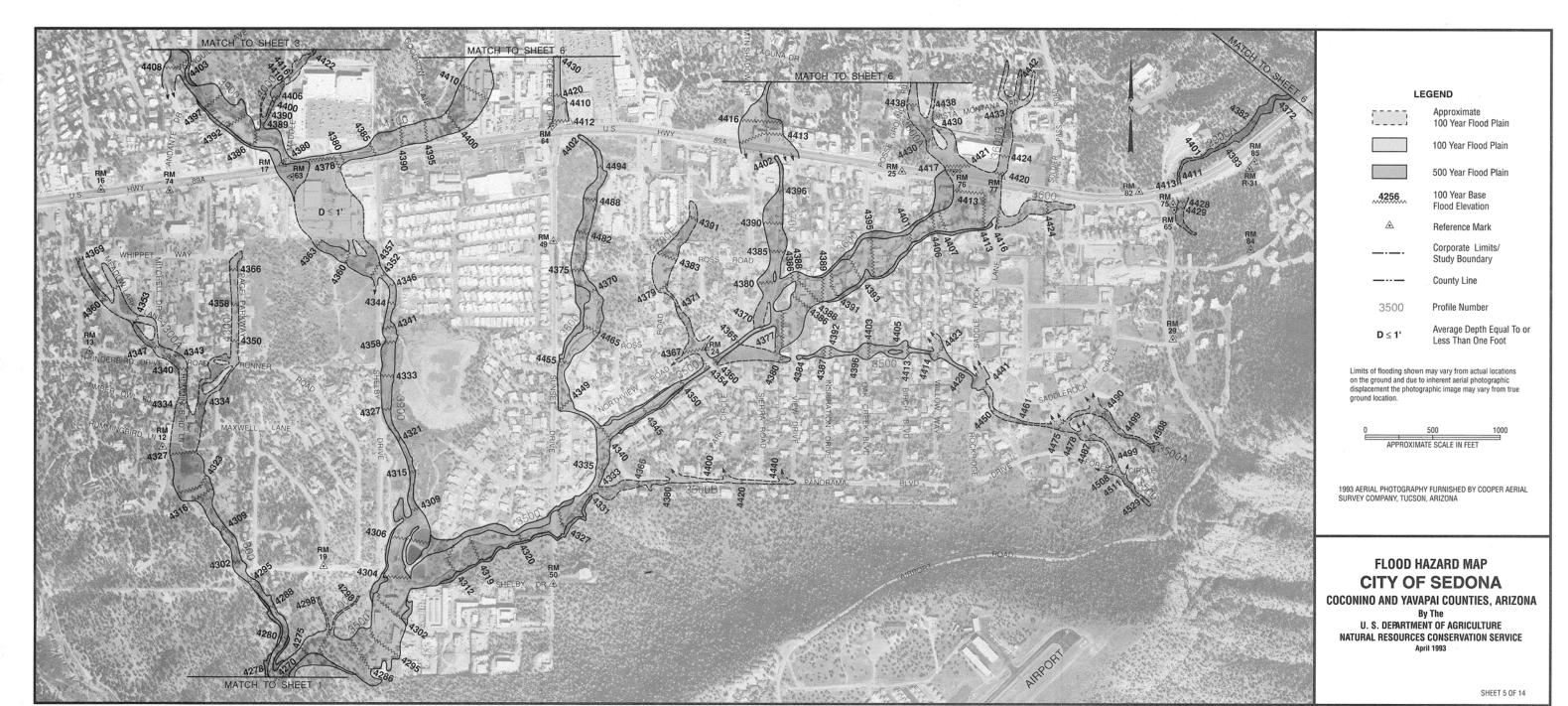
| + | 3 COMBINED AT | B50C | 628. | 12.10 | 65. | 21. | 10. | .36 |
|---|---------------|-------|-------|-------|------|------|-----|------|
| + | ROUTED TO | B50R | 603. | 12.20 | 65. | 21. | 10. | .36 |
| + | HYDROGRAPH AT | в61в | 46. | 12.05 | 4. | 1. | 0. | .03 |
| + | ROUTED TO | B61R | 44. | 12.10 | 4. | 1. | 0. | .03 |
| + | HYDROGRAPH AT | в60в | 165. | 12.00 | 16. | 5. | 2. | .07 |
| + | 2 COMBINED AT | B60C | 196. | 12.00 | 19. | 6. | 3. | .10 |
| + | ROUTED TO | B60R | 185. | 12.15 | 19. | 6. | 3. | .10 |
| + | HYDROGRAPH AT | в59в | 271. | 12.05 | 31. | 10. | 5. | .14 |
| + | 2 COMBINED AT | B59C | 422. | 12.10 | 50. | 16. | 8. | .24 |
| + | ROUTED TO | B59R | 424. | 12.10 | 50. | 16. | 8. | .24 |
| + | HYDROGRAPH AT | A34B | 350. | 11.90 | 20. | 6. | 3. | .12 |
| | DIVERSION TO | | | .00 | 20. | 6. | 3. | |
| + | HYDROGRAPH AT | D1 | 350. | | | | | .12 |
| + | ROUTED TO | DO1 | 0. | .00 | 0. | 0. | 0. | .12 |
| + | NOOTHD TO | A34R | 0. | .00 | 0. | 0. | 0. | .12 |
| + | HYDROGRAPH AT | B48B | 327. | 12.05 | 36. | 12. | 6. | .16 |
| + | 4 COMBINED AT | B48C | 1214. | 12.15 | 150. | 49. | 23. | .87 |
| + | ROUTED TO | B48R | 1206. | 12.20 | 150. | 49. | 23. | .87 |
| + | HYDROGRAPH AT | в47в | 236. | 11.95 | 20. | 7. | 3. | .09 |
| + | 2 COMBINED AT | B47C | 1238. | 12.20 | 170. | 55. | 27. | .96 |
| + | ROUTED TO | B47R | 1225. | 12.25 | 170. | 55. | 27. | .96 |
| + | HYDROGRAPH AT | B45B | 380. | 12.00 | 32. | 10. | 5. | .17 |
| + | HYDROGRAPH AT | B46B | 214. | 12.00 | 19. | 6. | 3. | .09 |
| + | 4 COMBINED AT | B45C | 3803. | 12.15 | 510. | 165. | 79. | 2.73 |
| + | ROUTED TO | B45R | 3764. | 12.20 | 510. | 165. | 79. | 2.73 |
| + | HYDROGRAPH AT | B42AB | 89. | 11.90 | 6. | 2. | 1. | .03 |
| + | ROUTED TO | | 80. | | | 2. | 1. | |
| + | HYDROGRAPH AT | | 85. | | 7. | 2. | 1. | .03 |
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SECTION F.2B Coffee Pot HEC-1 Model Summary Output (100-Year, Future Condition)

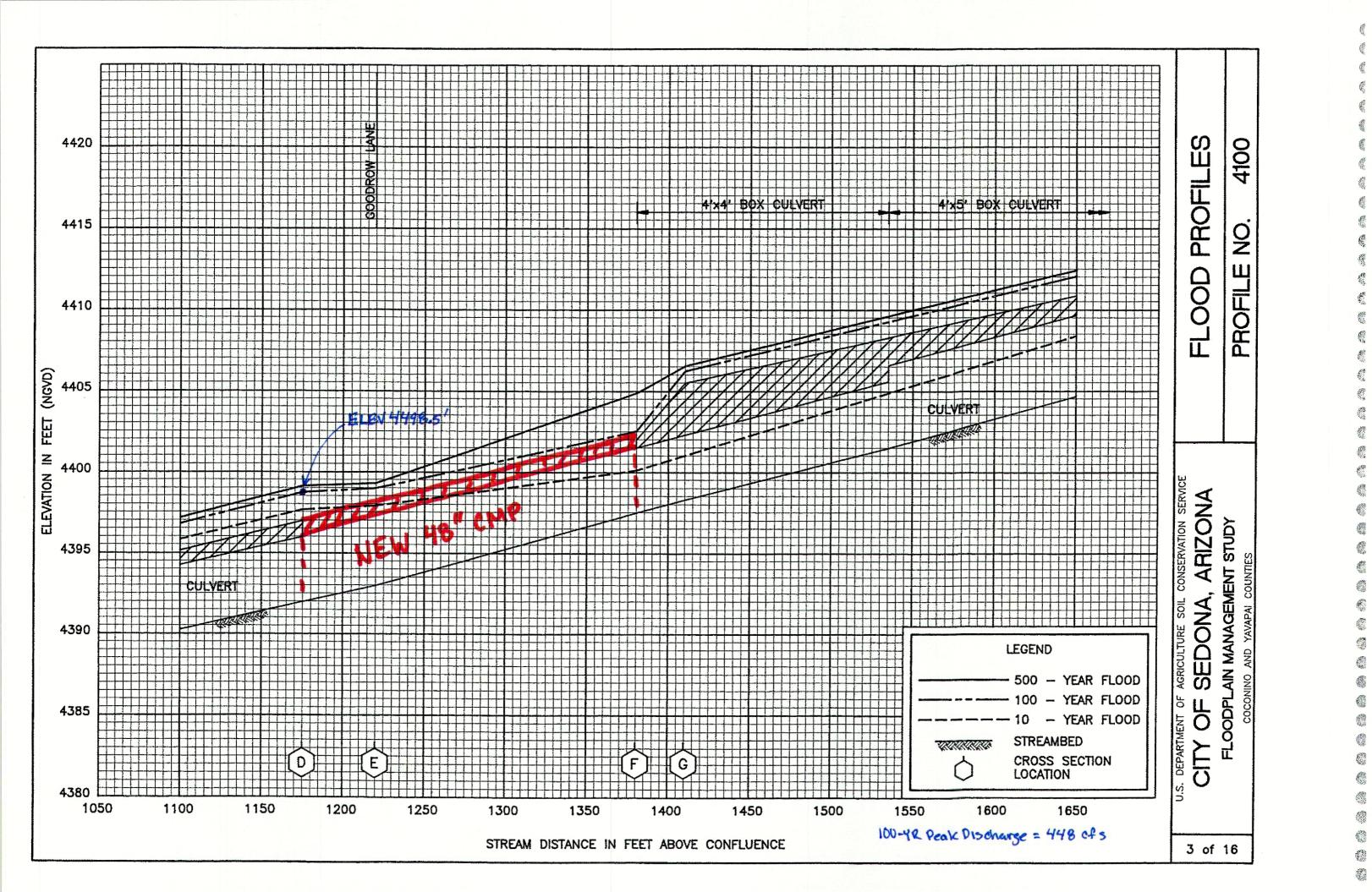
| + | 3 COMBINED AT | B50C | 849. | 12.05 | 86. | 27. | 13. | .36 |
|---|---------------|--------------|-------|-------|------|------|------|------|
| + | ROUTED TO | B50R | 810. | 12.20 | 86. | 27. | 13. | .36 |
| + | HYDROGRAPH AT | в61в | 61. | 12.05 | 5. | 1. | 1. | .03 |
| + | ROUTED TO | B61R | 59. | 12.10 | 5. | 1. | 1. | .03 |
| + | HYDROGRAPH AT | в60в | 212. | 12.00 | 20. | 7. | 3. | .07 |
| + | 2 COMBINED AT | B60C | 259. | 12.00 | 25. | 8. | 4. | .10 |
| + | ROUTED TO | B60R | 245. | 12.15 | 25. | 8. | 4. | .10 |
| + | HYDROGRAPH AT | в59в | 348. | 12.05 | 39. | 13. | 6. | .14 |
| + | 2 COMBINED AT | B59C | 565. | 12.05 | 64. | 21. | 10. | .24 |
| + | ROUTED TO | B59R | 568. | 12.10 | 64. | 21. | 10. | .24 |
| + | HYDROGRAPH AT | A34B | 451. | 11.90 | 27. | 8. | 4. | .12 |
| + | DIVERSION TO | D1 | 355. | 11.90 | 26. | 8. | 4. | .12 |
| + | HYDROGRAPH AT | DO1 | 96. | 11.90 | 1. | 0. | 0. | .12 |
| + | ROUTED TO | A34R | 45. | 12.00 | 1. | 0. | 0. | .12 |
| + | HYDROGRAPH AT | B48B | 422. | 12.05 | 46. | 15. | 7. | .16 |
| + | 4 COMBINED AT | B48C | 1706. | 12.10 | 197. | 63. | 30. | .87 |
| + | ROUTED TO | B48R | 1693. | 12.15 | 197. | 63. | 30. | .87 |
| + | HYDROGRAPH AT | в47в | 302. | 11.95 | 25. | 8. | 4. | .09 |
| + | 2 COMBINED AT | B47C | 1759. | 12.15 | 222. | 72. | 34. | .96 |
| + | ROUTED TO | B47R | 1745. | 12.20 | 222. | 72. | 34. | .96 |
| + | HYDROGRAPH AT | B45B | 491. | 12.00 | 42. | 13. | 6. | .17 |
| + | HYDROGRAPH AT | B46B | 277. | 12.00 | 24. | 8. | 4. | .09 |
| + | 4 COMBINED AT | B45C | 5362. | 12.10 | 666. | 213. | 103. | 2.73 |
| + | ROUTED TO | B45C B45R | 5328. | 12.10 | 666. | 213. | 103. | 2.73 |
| + | HYDROGRAPH AT | | 113. | 11.90 | 8. | 3. | | .03 |
| | ROUTED TO | B42AB | | | | | | |
| + | HYDROGRAPH AT | B42AR | 100. | 12.00 | 8. | 3. | 1. | .03 |
| + | | B42BB | 108. | 11.90 | 9. | 3. | 1. | .03 |

Appendix B

| City of Sedona Floodplain Management Study Excerpts | |
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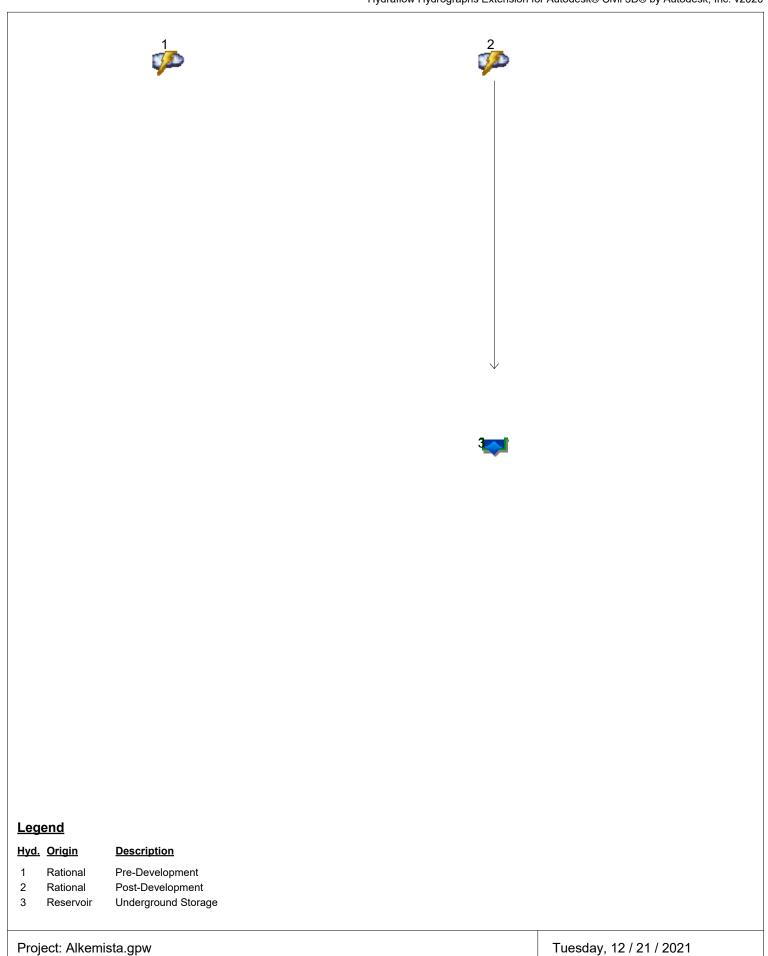
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Appendix C



Watershed Model Schematic



Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

| | Hydrograph | Inflow | | Peak Outflow (cfs) | | | | Hydrograph | | | |
|-----|------------------|--------|------|--------------------|------|-------|-------|------------|-------|--------|---------------------|
| No. | type (origin) | hyd(s) | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | Description |
| 1 | Rational | | | 1.283 | | 1.724 | 2.090 | 2.619 | 3.061 | 3.537 | Pre-Development |
| 2 | Rational | | | 1.991 | | 2.676 | 3.243 | 4.064 | 4.749 | 5.489 | Post-Development |
| 3 | Reservoir | 2 | | 1.206 | | 1.504 | 1.751 | 2.136 | 2.497 | 2.843 | Underground Storage |
| | | | | | | | | | | | |
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Proj. file: Alkemista.gpw

Tuesday, 12 / 21 / 2021

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description | | |
|---------------|--------------------------------|-----------------------|---------------------------|--------------------------|--------------------------|------------------------|------------------------------|-------------------------------|---------------------------|--|--|
| 1 | Rational | 2.090 | 1 | 10 | 1,254 | | | | Pre-Development | | |
| 2 | Rational | 3.243 | 1 | 10 | 1,946 | | | | Post-Development | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| Alkemista.gpw | | | | | Return F | Return Period: 10 Year | | | Tuesday, 12 / 21 / 2021 | | |

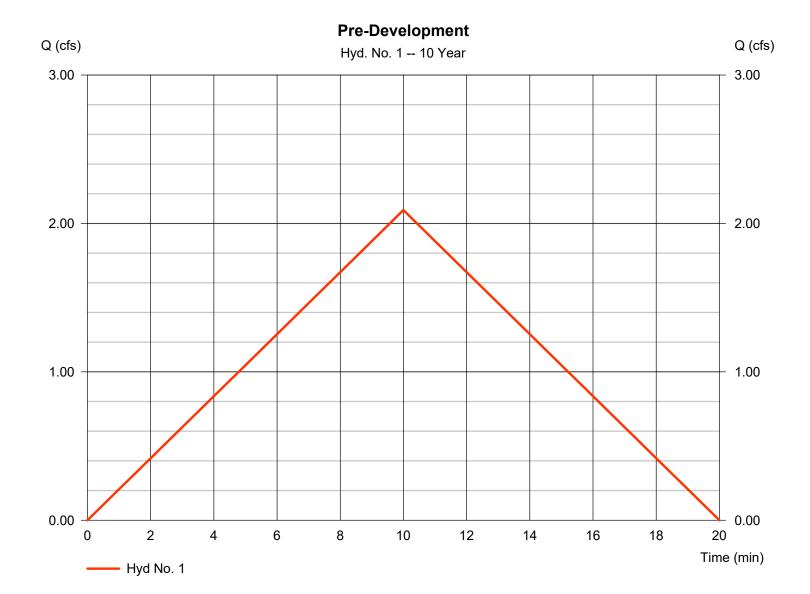
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Tuesday, 12 / 21 / 2021

Hyd. No. 1

Pre-Development

Hydrograph type Peak discharge = 2.090 cfs= Rational Storm frequency = 10 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 1,254 cuft Drainage area Runoff coeff. = 0.870 ac= 0.58Tc by User $= 10.00 \, \text{min}$ Intensity = 4.142 in/hrIDF Curve = Sedona.IDF Asc/Rec limb fact = 1/1



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

= 4.142 in/hr

Tuesday, 12 / 21 / 2021

= 10.00 min

Hyd. No. 2

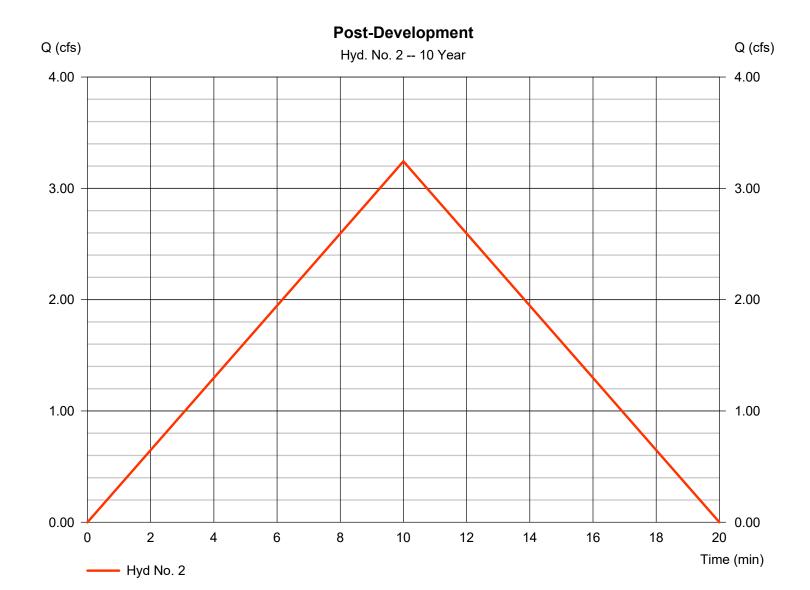
Intensity

Post-Development

Hydrograph type Peak discharge = 3.243 cfs= Rational Storm frequency = 10 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 1,946 cuft

Drainage area Runoff coeff. = 0.870 ac= 0.9Tc by User

IDF Curve = Sedona.IDF Asc/Rec limb fact = 1/1



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

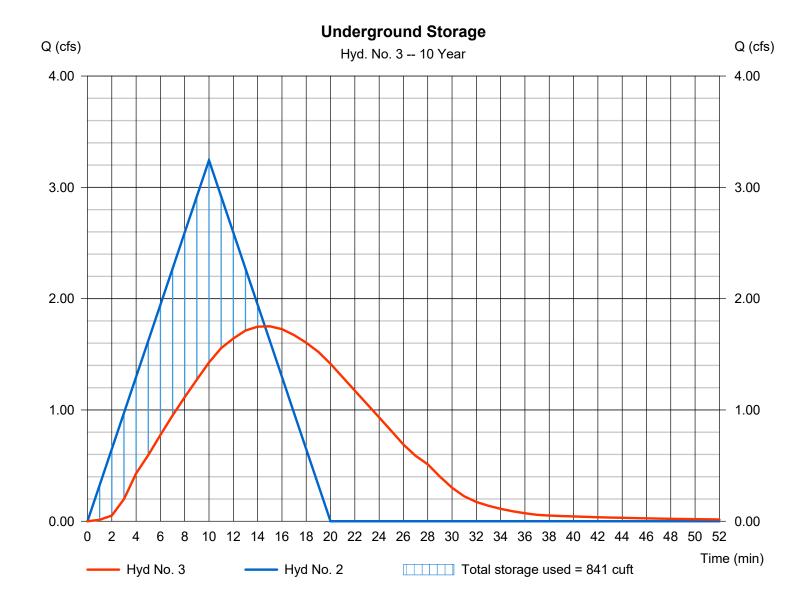
Tuesday, 12 / 21 / 2021

Hyd. No. 3

Underground Storage

= 1.751 cfsHydrograph type = Reservoir Peak discharge Storm frequency = 10 yrsTime to peak = 15 min Time interval = 1 min Hyd. volume = 1,945 cuftMax. Elevation Inflow hyd. No. = 2 - Post-Development = 4395.02 ftReservoir name = DB-1 Max. Storage = 841 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Tuesday, 12 / 21 / 2021

Pond No. 1 - DB-1

Pond Data

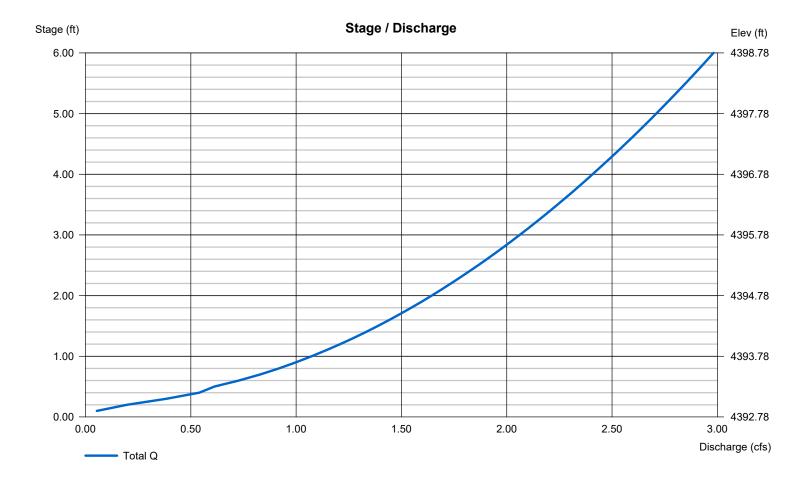
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 4392.78 ft. Voids = 40.00%

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 4392.78 | 965 | 0 | 0 |
| 1.00 | 4393.78 | 965 | 386 | 386 |
| 2.00 | 4394.78 | 965 | 386 | 772 |
| 3.00 | 4395.78 | 485 | 290 | 1,062 |
| 4.00 | 4396.78 | 485 | 194 | 1,256 |
| 5.00 | 4397.78 | 485 | 194 | 1,450 |
| 6.00 | 4398.78 | 485 | 194 | 1,644 |

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 4.00 6.00 0.00 = 0.00 0.00 0.00 0.00 Rise (in) 0.00 Crest Len (ft) Span (in) = 4.006.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels 0 Weir Coeff. = 3.333.33 3.33 3.33 Invert El. (ft) = 4392.784392.78 0.00 0.00 Weir Type = ---Length (ft) = 20.0020.00 0.00 0.00 Multi-Stage No = No No No Slope (%) = 1.001.00 0.00 n/a N-Value = .013 .013 .013 n/a = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) Orifice Coeff. Multi-Stage = n/a No No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|-------------|--------------------------------|-----------------------|---------------------------|--------------------------|--------------------------|------------------|------------------------------|-------------------------------|---------------------------|
| 1 | Rational | 3.537 | 1 | 10 | 2,122 | | | | Pre-Development |
| 2 | Rational | 5.489 | 1 | 10 | 3,293 | | | | Post-Development |
| 3 | Reservoir | 2.843 | 1 | 15 | 3,293 | 2 | 4398.26 | 1,543 | Underground Storage |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| Alk | emista.gpw | | | | Return F | Period: 100 | Year | Tuesday, 1 | 12 / 21 / 2021 |

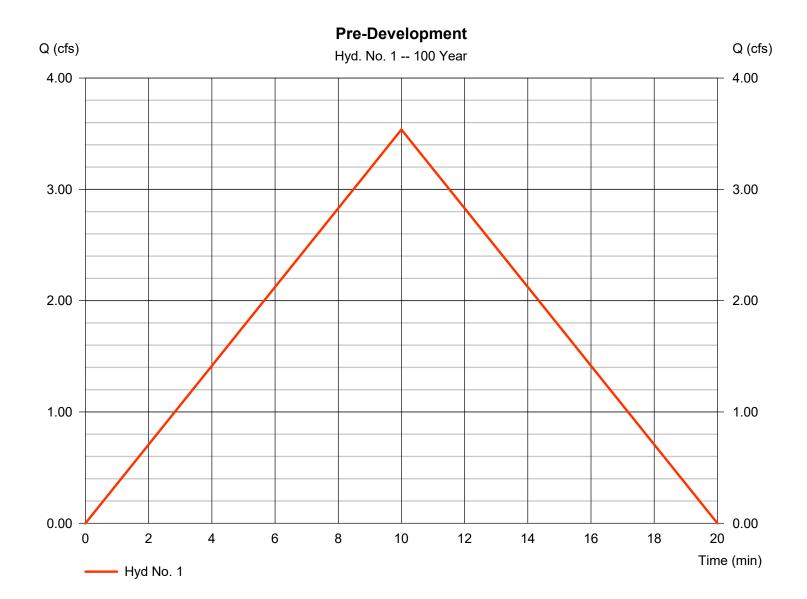
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Tuesday, 12 / 21 / 2021

Hyd. No. 1

Pre-Development

Hydrograph type Peak discharge = 3.537 cfs= Rational Storm frequency = 100 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 2,122 cuft Drainage area Runoff coeff. = 0.870 ac= 0.58= 7.010 in/hrTc by User = 10.00 min Intensity IDF Curve = Sedona.IDF Asc/Rec limb fact = 1/1



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

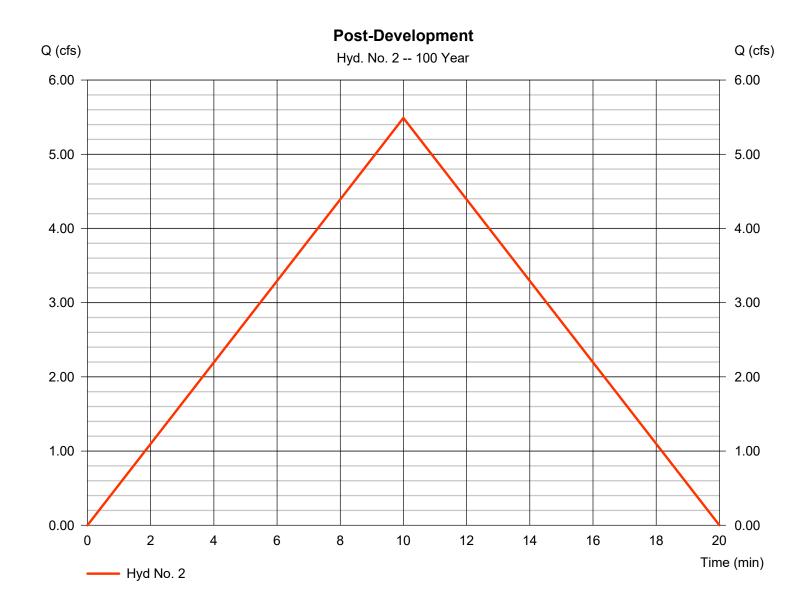
Tuesday, 12 / 21 / 2021

Hyd. No. 2

Post-Development

Hydrograph type Peak discharge = Rational = 5.489 cfsStorm frequency = 100 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 3,293 cuftRunoff coeff. Drainage area = 0.870 ac= 0.9Tc by User Intensity = 7.010 in/hr= 10.00 min

IDF Curve = Sedona.IDF Asc/Rec limb fact = 1/1



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

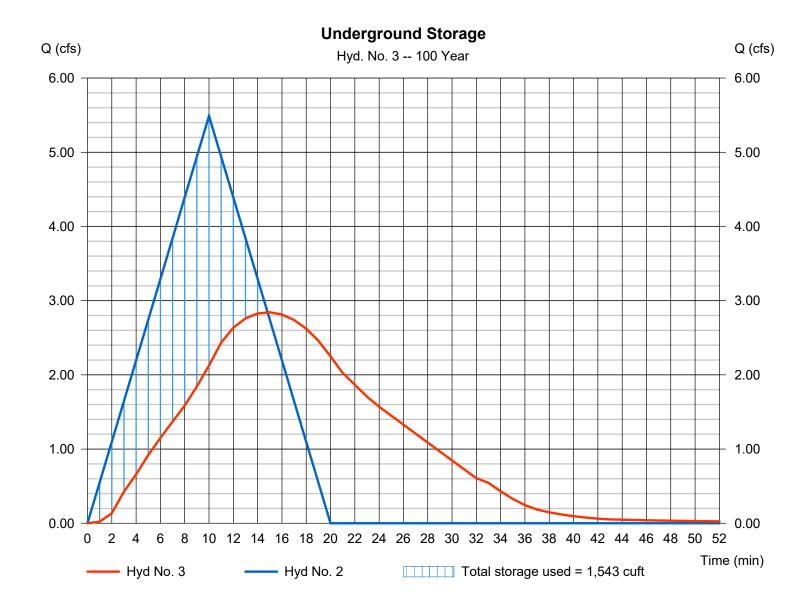
Tuesday, 12 / 21 / 2021

Hyd. No. 3

Underground Storage

Hydrograph type = Reservoir Peak discharge = 2.843 cfsStorm frequency Time to peak = 15 min = 100 yrsTime interval = 1 min Hyd. volume = 3,293 cuft Max. Elevation Inflow hyd. No. = 2 - Post-Development = 4398.26 ft Reservoir name = DB-1 Max. Storage = 1,543 cuft

Storage Indication method used.



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Tuesday, 12 / 21 / 2021

| Return Period | , | | | | | | | | | |
|------------------|---|--------|--------|-------|--|--|--|--|--|--|
| (Yrs) | В | D | E | (N/A) | | | | | | |
| 1 | 0.0000 | 0.0000 | 0.0000 | | | | | | | |
| 2 | 30.5834 | 9.1000 | 0.8432 | | | | | | | |
| 3 | 0.0000 | 0.0000 | 0.0000 | | | | | | | |
| 5 | 39.8064 | 8.9000 | 0.8353 | | | | | | | |
| 10 | 47.9118 | 8.9000 | 0.8330 | | | | | | | |
| 25 | 61.3299 | 9.0000 | 0.8387 | | | | | | | |
| 50 | 70.5549 | 8.9000 | 0.8349 | | | | | | | |
| 100 | 83.5403 | 9.1000 | 0.8401 | | | | | | | |

File name: Sedona.IDF

Intensity = B / (Tc + D)^E

| Return Period (Yrs) | Intensity Values (in/hr) | | | | | | | | | | | |
|---------------------------|--------------------------|------|------|------|------|------|------|------|------|------|------|------|
| | 5 min | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 3.28 | 2.54 | 2.09 | 1.78 | 1.56 | 1.39 | 1.26 | 1.15 | 1.06 | 0.98 | 0.92 | 0.86 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 4.42 | 3.42 | 2.81 | 2.40 | 2.10 | 1.87 | 1.69 | 1.54 | 1.42 | 1.32 | 1.24 | 1.16 |
| 10 | 5.35 | 4.14 | 3.41 | 2.91 | 2.55 | 2.27 | 2.05 | 1.88 | 1.73 | 1.61 | 1.50 | 1.41 |
| 25 | 6.71 | 5.19 | 4.27 | 3.64 | 3.19 | 2.84 | 2.57 | 2.35 | 2.16 | 2.01 | 1.87 | 1.76 |
| 50 | 7.84 | 6.07 | 4.99 | 4.25 | 3.72 | 3.32 | 3.00 | 2.74 | 2.53 | 2.35 | 2.19 | 2.06 |
| 100 | 9.05 | 7.01 | 5.77 | 4.92 | 4.31 | 3.84 | 3.47 | 3.17 | 2.92 | 2.71 | 2.54 | 2.38 |

Tc = time in minutes. Values may exceed 60.

Precip. file name: Sample.pcp

| | Rainfall Precipitation Table (in) | | | | | | | | | |
|-----------------------|-----------------------------------|------|------|------|-------|-------|-------|--------|--|--|
| Storm Distribution | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | | |
| SCS 24-hour | 0.00 | 2.20 | 0.00 | 3.30 | 4.25 | 5.77 | 6.80 | 7.95 | | |
| SCS 6-Hr | 0.00 | 1.80 | 0.00 | 0.00 | 2.60 | 0.00 | 0.00 | 4.00 | | |
| Huff-1st | 0.00 | 1.55 | 0.00 | 2.75 | 4.00 | 5.38 | 6.50 | 8.00 | | |
| Huff-2nd | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Huff-3rd | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Huff-4th | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Huff-Indy | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Custom | 0.00 | 1.75 | 0.00 | 2.80 | 3.90 | 5.25 | 6.00 | 7.10 | | |

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Tuesday, 12 / 21 / 2021

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Appendix D

Grading and Drainage Plan